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PREPARATION AND CHARACTERIZATION OF SOLID LIPID NANOPARTICLES THROUGH RAPID EXPANSION OF SUPERCRITICAL SOLUTION

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ABSTRACT: Rapid expansion of supercritical solution (RESS) has provided a promising alternative to produce ultrafine particles of heatsensitive materials. Stearic acid is a good lipid for development of solid lipid nanoparticles (SLNs) in drug delivery systems. Therefore, currently, much research on the micronization of stearic acid is going on. In this study, formation of submicron stearic acid was reported by using RESS process. Thanks to high solubility of stearic acid in supercritical CO2, RESS can be used to produce stearic acid nanoparticles and so in this process, extraction temperature and pressure are a bit more than critical point of SC-CO2. The unprocessed and processed stearic acid powders were characterized by means of scanning electron microscopy (SEM), X-ray diffraction (XRD), differential scanning calorimetry (DSC) and Fourier transform infrared spectrophotometry (FT-IR). FT-IR analysis and XRD pattern of processed stearic acid showed that the degree of crystallinity was reduced without any chemical structural change. DSC analysis showed a 2.7°C decrease in the melting point from that of bulk stearic acid. Also, the RESS processing of stearic acid leads to spherical particles in the range from40nm to 200 nm which are about 600 times smaller than the unprocessed powder as reflected by SEM observations.

INTRODUCTION: Supercritical fluid technology has been widely used for various applications such extraction, reaction, chromatography as and processing. material The most important characteristic of particle formation from supercritical fluid technology is the possibility of producing solids with unique morphology and small size.



understanding of However the applying supercritical fluid to particle formation is still in their infancy ¹. Several papers have been published about the applications of supercritical fluid on the preparation of nano-materials²⁻⁴. Supercritical fluids (SCF) have several properties such as high diffusivity, low viscosity, and high compressibility. These make them attractive solvents for many industrial processes. Supercritical CO₂(SC-CO₂) is the most popular SCF, because it is non-toxic, nonflammable, easy to obtain and has a near-ambient critical temperature ⁵. Small changes in the temperature or pressure near the critical point result in significant changes in the solubilizing power of supercritical fluid and in turn density.

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Therefore, density depends on the applied temperature and pressure.

Currently, two common routes for particle formation in supercritical fluids are available: supercritical antisolvent process (SAS)⁶⁻⁸ and rapid expansion of supercritical solutions (RESS)⁹⁻¹¹. In SAS process, the solute of interest is dissolved in the organic solvent and then the solution is sprayed into an excess of antisolvent. While the solubility of the solute in the antisolvent is limited, the organic solvent is miscible with the antisolvent. Under contacting conditions, high mass transfer rates occur. It leads to the formation of solid microparticles¹².

The RESS process consists of two steps. The first step is an extraction in which the supercritical fluid is saturated with the substrates of interest. This extraction is followed by a sudden depressurization in a nozzle which produces a large decrease in the solvent power and the temperature of the fluid, therefore causing the precipitation of the solute. The morphology of the resulting product, crystalline or amorphous, depends on the chemical structure of the material and on the RESS parameters (temperature, pressure drop, impact distance of the jet against a surface, nozzle geometry, etc...)³.

This process can be applied to micronize non-polar compounds soluble in SC-CO₂¹³. RESS process omits the problems of the conventional micronization methods to produce small particles with narrow particles size distribution (PSD)¹⁴. Stearic acid is a saturated fatty acid, with 18 carbon-chain length and a high lipophilic character (**Figure 1**). It is often selected as solid lipid for the production of lipid nanoparticle dispersions¹⁵.

Stearic acid, like other lipids and related long-chain compounds, may crystallize in different polymorphic forms depending on the conditions in which the crystallization is performed ¹⁶.



FIG. 1: CHEMICAL STRUCTURE OF STEARIC ACID

Stearic acid as a SLN allows a high drug loading by the less ordinate structure of the lipid matrix. The other advantages of SLNs include: controlled and targeted drug release, feasibility of carrying both hydrophilic and lipophilic drug, improved drug stability, easy to scale up and sterilize ¹⁷⁻²⁰. Hence, due to its extensive application in drug delivery system, preparation and characterization of stearic acid nanoparticles was studied.

The solubility of solutes in supercritical CO2 is probably the most important property that is needed to be known for the production of micronized solutes by RESS. Solubility of stearic acid in pure SCF CO2 is reported in literature ²¹⁻²³. Because of good solubility in SCF CO2, RESS can be used to produce stearic acid nanoparticle (**Table 1**) The aim of the present study is formation of ultrafine stearic acid by using RESS method as a good lipid for development of SLN application, and also to characterize the physicochemical properties of obtained samples, such as surface properties, crystallinity, morphology, chemical behavior and chemical structure.

| Temperature (°C) | Pressure (bar) | Solubility (*10 ⁻⁴) |
|---------------------|----------------|---------------------------------|
| | 128.5 | 0.74 |
| | 148.1 | 0.89 |
| 35 | 167.7 | 1.03 |
| | 197.1 | 1.19 |
| | 226.5 | 1.24 |
| | 128.5 | 0.83 |
| | 148.1 | 1.48 |
| 45 | 167.7 | 2.12 |
| | 197.1 | 2.87 |
| | 226.5 | 3.24 |

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MATERIALS AND METHODS:

Materials: Stearic acid (SA, purity: 99.9%, MW: 284.48, Merck Chemical Co.) was used for particles production. Carbon Dioxide with the purity of 99.99% was purchased from Farafan Gas Company which was used as extracting agent. Potassium Bromide was supplied from Merck. It should be stated that all the chemicals were used as received without any further purification.

Apparatus: The RESS apparatus is shown schematically in **Figure 2**. The system is consisted of two sections: extraction and precipitation. In order to keep the temperatures of the equilibrium cells constant, a high accurate temperature-controlled water bath with an uncertainty of $\pm 0.1^{\circ}$ C was used (Type WPE 45, Memmert Germany). The capacity of the equilibrium cells placed in the water bath, vessels 4 and 5 in the schematic diagram, was 200 and 300 cm³, respectively. The body of the

equilibrium cells, valves, and tubes were all made of stainless steel and supplied from Swagelok Company (USA). Two vessels were used in series in order to ensure achieving equilibrium condition. The cells were filled with stearic acid at various temperature and pressure. The pressure of the cells was measured with a digital pressure transducer with an uncertainty of ±0.1MPa (Type KM11, Ashcroft instruments, Germany). The purified gaseous CO2 is liquefied and sub-cooled in a chiller and afterwards compressed to the desired pressure with a reciprocating pump type SFT-10 (Supercritical fluid technologies INC., USA). Sinter metal filter was used on both ends of the vessels 4 and 5 to avoid flooding of the undissolved material imposed by CO₂ flow. Preheating coils and the extraction vessel were immersed at constant temperature water bath. As shown in Fig. 2, the precipitation unit consists of a cell, an expansion device and a collection device. Equipment of material is made of aluminum.



(1) CO_2 tank, (2) pump, (3) heat exchanger, (4, 5) equilibrium vessels, (6) constant temperature water bath, (7) preheating tube, (8) expansion device, (9) precipitation unit, (10) collection sample holder, (11) refrigerated water bath circulator, (12) data acquisition system (TI: temperature indicator; TIC: temperature indicator controller; PI: pressure indicator).

The main part of the expansion device is nozzle (SITEC Co., Switzerland). During rapid expansion and in order to avoid freezing and plugging within the nozzle that is heated by a cartridge heater, which is controlled by a PID controller (Type TPR-2N, Han Young NUX Co., Republic of Korea). The temperature of the gas flowing through the nozzle was measured by a thermocouple (J-type) and a digital display (Type TPR-2N, Han Young NUX

Co., Republic of Korea). The thermocouple was placed precisely into the solution stream approximately 7mm above the entrance region of the nozzle. A highly accurate temperaturecontrolled refrigerated water bath was used to keep the temperature of the precipitation unit constant (Type WCL-P8, Daihan Scientific Co., Republic of Korea). The collection device, by which the precipitated particles are collected, is placed inside

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the precipitation cell. The top part of the collection device, namely the collection table, is made of Teflon. For collection of the particles, the glass slides are located on this table. The spray distance (the distance between the tip of the nozzle and the surface of the glass slide) can be changed via adjustable bolt and nut mechanism. In previous studies, this apparatus has been used for nanoparticles production^{14, 25}.

Characterization:

Scanning Electron Microscopy analysis (SEM): The morphology and size of the precipitated particles were examined by SEM (KYKY, EM-3200, and China). For analysis, the particles were attached to the carbon tape that is on the top of SEM aluminum stubs and were then coated with gold using a sputter coater.

Determination of the particles size distribution was performed with the CLEMEX particles imageanalysis package. The SEM figures which were taken from the collected glass slide were introduced to the image processing software. All SEM analyses were done at accelerating voltage of 24 and 26 kV. **X-Ray Diffraction Analysis (XRD):** To study the polymorphism and crystalline properties of the lipid, XRD was carried out in a diffractometer X-ray (Philips, model Xpert PW3040/60, Netherlands). The conditions were: 40 kV voltages; 30 mA current; at room temperature. The samples were loaded on to the diffractometer and scanned over a range of 2θ values form 10 to 100at a scan rate of 0.020° / sec.

Fourier Transform Infrared Spectrophotometer analysis (FTIR): Chemical analysis of unprocessed and RESS processed stearic acid particles were performed by Fourier Transform Infrared (FTIR) spectrophotometer (Bruker-Tenasor 27, Germany). About 1–2 mg of sample was mixed with dry potassium bromide and the samples were examined at transmission mode over wave number range of 4,000 to 400 cm⁻¹.

Differential scanning calorimetry Analysis (**DSC**): Thermal behavior of lipid matrices was assessed by DSC and it was performed using DSC Q100 (Mettler Toledo, DSC1, Switzerland). For DSC measurement, 10 mg of powdered stearic acid nanoparticles were put in 40 μ l aluminum pans. A scan rate of 10°C/min was employed in the 0–200°C temperature range.

| Run no. | Extraction temperature (°C) | Extraction pressure (bar) | Pre-expansion temperature (°C) | Average particle size (µm) |
|----------|--------------------------------|------------------------------|-----------------------------------|-------------------------------|
| Original | - | - | - | 100 |
| 1 | 35 | 80 | 50 | 0.152 |
| 2 | 35 | 100 | 50 | 0.142 |
| 3 | 40 | 100 | 50 | 0.66 |
| 4 | 40 | 100 | 80 | >2 |

TABLE 2: EXPERIMENTAL CONDITIONS AND RESULTS FOR THE STEARIC ACID IN RESS PROCESS

RESULTS AND DISCUSSION:

Particle formation: Summarized in Table 2 are experimental conditions carried out in this study. In each experiment, 2 g (additional material to ensure the attaining of equilibrium conditions) of stearic acid was charged into each equilibrium vessel. It is worth pointing out that glass granular beads were introduced into the equilibrium vessel in association with the chemicals to increase the contact surface area. Prior to running the experiments, entrapped air was purged out from the vessels and piping by CO_2 injection.

In all experiments, nozzle diameter is 45 μ and the spray distance is 5 cm and time of gathering precipitated stearic acid on glass slides is 20 min. The size and shape of precipitated particles were analyzed by scanning electron microscopy. The crystal structures and thermal behavior of original and precipitated stearic acid were examined using an X-ray-diffractiometer and differential scanning calorimeter, respectively. FTIR analysis was also used for chemical structure.



FIG. 3: The SEM images of (a) unprocessed stearic acid particles and processed stearic acid particles prepared by the RESS process (b) at extraction pressure of 80bar, extraction temperature of $35 \circ C$ and pre-expansion temperature of $50 \circ C$, (c) at extraction pressure of 100 bar, extraction temperature of $35 \circ C$ and pre-expansion temperature of $50 \circ C$, (d) at extraction pressure of 100 bar, extraction temperature of $35 \circ C$ and pre-expansion temperature of $50 \circ C$, (d) at extraction pressure of 100 bar, extraction temperature of $50 \circ C$ and pre-expansion temperature of $50 \circ C$, (d) at extraction pressure of 100 bar, extraction temperature of $50 \circ C$ and pre-expansion temperature of $50 \circ C$, (d) at extraction pressure of $100 \circ C$ and pre-expansion temperature of $50 \circ C$.

SEM analysis: For external morphology and shape, the formulation was characterized by scanning electron microscopy. Unprocessed stearic acid particles have an average size of 100 micrometer and are nearly spherical in shape illustrated in Figure 3a and 4a. After the RESS process, stearic acid samples which were subject to SC-CO₂ at the extraction temperature of 35° C, preexpansion temperature of 50°C and extraction pressure of 80 bar exhibits a smaller average diameter size of 152nm illustrated in Figure 3b and 4b. Therefore, the SEM image shows a modification on the morphology of the precipitated particles and they are in spherical shape after RESS processing. It is quite evident that there is a slight change in the particle morphology and a sharp decrease in particle size after processing with RESS. However, under the same treatment condition but with a further increase in the extraction pressure to 100 bars, a lower average diameter size of 142 nm could be achieved for stearic acid nanoparticles with similar appearance as illustrated in Figure 3c and 4c. Results reveal that there is no significant change in the average diameter size of stearic acid but it is less agglomerated. This could be explained by the following two aspects.

Firstly, the concentration of solution was increased by increasing the extraction pressure; therefore, according to the classical nucleation theory, higher concentration of solution made a decrease of particle size ²⁶. Secondly, a higher pre-expansion pressure led to higher mass flow rates of the solution (it should be to state that in our experiments, the pre-expansion pressure was kept equal to the extraction pressure). Consequently, higher mass flow rates of the solution reduced the residence time in the expansion chamber, which was the particle coagulation growth time. Both phenomena were responsible for the decrease of particle size ¹⁴.



FIG. 4: Particle size distribution of (a) unprocessed stearic acid particles and processed stearic acid particles prepared by the RESS process (b) at extraction pressure of 80 bar, extraction temperature of $35 \circ C$ and pre-expansion temperature of $50 \circ C$, (c) at extraction pressure of 100 bar, extraction temperature of $35 \circ C$ and pre-expansion temperature of $50 \circ C$, (d) at extraction pressure of 100 bar, extraction temperature of $35 \circ C$ and pre-expansion temperature of $50 \circ C$, (d) at extraction pressure of 100 bar, extraction temperature of $50 \circ C$, (d) at extraction pressure of 100 bar, extraction temperature of $50 \circ C$, (d) at extraction pressure of 100 bar, extraction temperature of $50 \circ C$, (d) at extraction pressure of $100 \circ C$ and pre-expansion temperature of $50 \circ C$, (d) at extraction pressure of $100 \circ C$ and pre-expansion temperature of $50 \circ C$, (d) at extraction pressure of $100 \circ C$ and pre-expansion temperature of $50 \circ C$, (d) at extraction pressure of $100 \circ C$ and pre-expansion temperature of $50 \circ C$.

An increase in extraction temperature from 35°C to 40°C caused a decrease of average particles size. This could be explained as follows. Increasing the extraction temperature leads to reduce the density of CO2 and simultaneous increase in the solutes vapor pressure. In addition, reduction in the solvent density causes a decrease in the solvent power. On the other hand, increase in the solutes vapor pressure leads to an increase in the stearic acid solubility.

Therefore, the total effect of the two opposing phenomena increases the solubility of stearic acid in the supercritical fluid ^{14, 26 and 27}. Therefore, high extraction temperature induces high stearic acid solubility at a constant extraction pressure and leads to increase in the supersaturation. According to classical nucleation theory, the increase of supersaturation leads to decrease in critical nucleus size and therefore the smaller particles were obtained ^{14, 28–31}. Huang *et al* ¹ reported the similar result for aspirin. Also, our results reveal that an increase in the extraction temperature to 40°C and extraction pressure of 100 bar result in a decrease

in the average particle sizes but the agglomeration happened rather quickly and the final products were in fact largely aggregates of nanoscale particles as shown in **Fig. 3d and 4d**. The resultant trend in these series of experiments could be related to the solubility of stearic acid in supercritical carbon dioxide. In evaluation of agglomeration of stearic acid particles, it could be noted that high solubility leads to presence of more particles which provide the situation for them to be in contact. This agglomeration of particles occurred in expansion zone as the particles have ample time to collide with each other and coagulate to form bigger particles.

Hence, these results would show that further increase in extraction pressure and decrease in extraction temperature would decrease particle size but cause the more agglomeration of stearic acid nanoparticles, attributed to increase of stearic acid solubility in supercritical CO₂. Therefore, due to high solubility of stearic acid in supercritical CO₂, extraction temperature and pressure have been applied a bit more than critical point of SC-CO₂.

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Compared to traditional RESS processes, this process will be more efficient and cost saving when is used for production of solid lipid nanoparticles in large scale. Hence, production of drug loaded solid lipid nanoparticles with different drugs through RESS process is part of our current research activities.



FIG. 5: The SEM images of processed stearic acid particles prepared by the RESS process at extraction pressure of 100bar, extraction temperature of 35°C and pre-expansion temperature of 80°C

The pre-expansion temperature for stearic acid in this study ranges from 50° C to 80° C. As shown in **Fig. 5**, when pre-expansion temperature is more than the melting temperature of stearic acid; liquid droplets were formed and quickly solidified within the expansion unit and leads to form larger particles (more than 2 µm). Therefore, pre-expansion temperature should be less than melting temperature of micronized stearic acid.

X-Ray Diffraction: X-ray powder diffraction is a rapid analytical technique primarily used for phase identification of a crystalline material. Small changes in the X-ray powder patterns due to the appearance of new peak(s), additional shoulders or

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shifts in the peak position may imply the presence of a new polymorph. In this study, the XRD patterns for the unprocessed stearic acid particles are given in Fig. 6(a) which exhibits sharp peaks at 20 scattered angles 20.92 and 23.32. This is an indication of a crystalline nature of stearic acid. Sharp peaks for micronized stearic acid were exhibits at 2θ scattered angles 21.48 and 23.72, respectively. XRD analysis patterns for Figure 6a and 6b are nearly at the same angles and the intensity of the peaks are lower for the RESS processed particles of stearic acid. Lower intensity can be attributed to lowering of crystallinity of the particles. Formation of the nanoparticles can be another reason for lowering the intensity. In other words, both the unprocessed and the stearic acid nanoparticles showed approximately similar X-ray diffraction patterns. This implies that the crystalline form of the micronized stearic acid was approximately unchanged by the RESS process.





FIG. 6: X-RAY POWDER DIFFRACTOGRAM OF (a) stearic acid unprocessed starting material and (b) processed stearic acid particles prepared by the RESS method at extraction pressure of 100 bar, extraction temperature of $40 \circ C$ and pre-expansion temperature of $50 \circ C$

Stearic acid exhibits polymorphism, which is defined as the ability of a substance to exist in two or more crystalline phases. Stearic acid has four polymorphs: *A*, *B*, *C* and *E*. Polymorph *A* is triclinic, whereas forms *B*, *C* and *E* are monoclinic. The C form is thermodynamically most stable in the high temperature region (> 32 °C) and *A* and *B* forms transform to the C form irreversibly ³².

X-ray diffraction of A, B and C polymorph and their mixture were studied by Garti *et al* ³³. Their results show that C polymorph shows two strong peaks at 2 θ scattered angles between 20 and 25.

Therefore, Fig. 6(a) and 6(b) reveals that unprocessed and micronized stearic acid may be in C form and there is no any change in crystal structure of stearic acid under high pressure in RESS process.

FT-IR analysis: FT-IR spectroscopy was employed to obtain conformational information about the lipid molecule. In regard to chemical structure of stearic acid, it is shown that stearic acid is composed of two important sections; carboxylic head (COOH) and hydrocarbon tail. The principle FT-IR peak (Figure 7) of unprocessed stearic acid obtained at $1,701 \text{ cm}^{-1}$ is due to the absorption of C=O stretching group. The FT-IR spectrum shows the other characteristic peak of stearic acid such as hydrogen-bonded O-H stretching at 2849cm⁻ which have obscured other peaks in this region.

The other principal peaks respectively, are obtained 2918 cm⁻¹ (C-H stretching) and 1424 cm⁻¹ - 1500 cm⁻¹ (C-H bend). As illustrated in **Figure 8**, in the spectrum of micronized stearic acid, principal peaks were obtained at1702 cm⁻¹ (C=O stretching), 2850 (hydrogen-bonded O-H Stretching) and 2919 cm⁻¹ (aliphatic C-H stretching). This indicates that there is no any change in chemical structure of stearic acid under high pressure in this process.



FIG 7: FT-IR ANALYSIS OF UNPROCESSED STEARIC ACID PARTICLES



FIG. 8: FT-IR ANALYSIS OF PROCESSED STEARIC ACID PARTICLES PREPARED BY THE RESS METHOD AT EXTRACTION PRESSURE OF 100BAR, EXTRACTION TEMPERATURE OF 40°C AND PRE-EXPANSION TEMPERATURE OF 50°C

The C polymorphic form shows a single strong IR band at 937 cm⁻¹ corresponding to the OH bending vibration band of the carboxyl group. Consequently, comparison of the FT-IR spectrum and XRD pattern of processed and unprocessed stearic acid (**Figure 6, 7 and 8**) with the published FT-IR spectrum of different polymorphic forms of stearic acid ³⁴ indicates that the crystal structure was unchanged and confirmed to be as polymorph form C before and after the RESS process.

DSC Analysis: Differential Scanning Calorimetry is a suitable thermal analysis technique for

determining the purity, the polymorphic forms, crystallinity and the melting point of lipids. The obtained nanoparticles were characterized by DSC analysis. **Figure 9** shows the heat flow with temperature plot of unprocessed and RESS processed stearic acid.

In **Figure 9a**, only one pronounced melting point peak of unprocessed SA at 57.3 °C was observed, different from literature of 69.6 °C of pure SA. Of course the same result with our study was presented for thermal behavior and melting point of unprocessed SA by Pawara ³⁴ and by Ribeiro ³⁵.



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FIG. 9: DSC ANALYSIS OF a) UNPROCESSED STEARIC ACID AND b) PROCESSED STEARIC ACID NANOPARTICLES PREPARED BY THE RESS PROCESS AT EXTRACTION PRESSURE OF 100 BAR, EXTRACTION TEMPERATURE OF 40°C AND PRE-EXPANSION TEMPERATURE OF 50°C

The DSC analysis of stearic acid nanoparticles showed a 2.7°C decrease in the melting point from that of bulk stearic acid and nanoparticles had the same melting behavior compared to unprocessed stearic acid in literature ³⁶. The lower melt point observed for processed stearic acid may be due to its lower crystallinity, which agrees with our XRD analysis. Because for the less-ordered crystal structure, the melting process requires less energy than the perfect crystalline substance to overcome lattice force.

Lipid crystallinity can be determined with DSC by measurement of the heat of fusion of the lipid. Percent of crystallinity is reported by normalizing the measured heat of fusion to that of a100 % crystalline sample of the same lipid. As standard enthalpy change of fusion of pure stearic acid is202.70kj/kg and normalized enthalpy change of fusion of micronized stearic acid is 189.19kj/kg, therefore stearic acid nanoparticles crystallinity is nearly 95%.

Hence, it has less effect on lowering melting point. Besides, lower melting point is possibly due to the fact that small particles obtained from the RESS have higher specific surface area leading to decrease in melting enthalpy. The thermodynamic relationship between of polymorphs of stearic acid can be studied by DSC analysis. Transition between polymorphs (for example polymorph A to polymorph C or polymorph B to polymorph C) exhibits a weak endothermic peak with a transition enthalpy. Any weak endothermic peak is not observed in DSC curves of unprocessed and micronized stearic acid.

Therefore, DSC analysis confirms that there are not two or more different polymorphs within unprocessed and micronized stearic acid. Hence, Xray diffraction and IR spectrum along with DSC reveals that product is composed of thermodynamically most stable polymorph C.

CONCLUSION: This work investigates the micronization of stearic acid by using RESS process of SC-CO₂. Our experimental results show that rapid expansion of stearic acid with SC-CO₂ could provide micronized particles.

The obtained stearic acid particles were within a range of micro-scaled with acceptably narrow size distribution. Anyway, based on our FT-IR analyses, no significant change in chemical composition of the micronized stearic acid particles was detected.

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In the results obtained for XRD of micronized stearic acid more diffuse and low intensity peaks were observed as compared to the sharper and high intensity peaks obtained for the bulk lipid.

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